AD 14184

ACCELERATED LIFE TESTING OF METALLIC PECTIFIERS

3rd QUARTERLY REPORT (January 1, March 31, 1953)

FACTORS AFFECTING LIFE CHARACTERISTICS
OF METALLIC RECTIFIERS

CONTRACT NO. DA-36-039 SC 42490

DEPARTMENT OF THE ARMY PROJECT NO. 3-99-15-022 SIGNAL CORPS PROJECT NO. 32-152 B

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1-0 Abstract

The present report describes the work done and the results achieved in the course ω an investigation aimed to develop an accelerated life testing procedure for Selenium Rectifiers.

Data on standard life tests, and on tests performed under higher than normal ambient temperature or higher than normal current density are included - for a total of 88 stacks.

2-0 Purpose

2-1 This study is aimed at the gathering of quantitative data to be used as a basis for the establishment of an accelerated life testing procedure for Selenium Rectifiers.

Under Specification MIL-R-11050, SGC, such testing is now performed at rated electrical loading at normal ambient temperature and requires 3000 hours (125 days) to establish adequacy of performance.

A method of evaluation more efficient with respect to the time is highly desirable for both military and industrial users of Selenium Rectifiers.

More specifically the principal objective of this study is the establishment of a procedure which will consent, through the use of curves, tables, or formulas, to extrapolate the long life behavior of Selenium Rectifiers from the results of a comparatively short test (200 hours).

The systematic gathering of life test data on a large number of rectifiers of different makes and dimensions, under different environmental and operating conditions alone may prove to be a useful by-product of the present investigations.

- 3-0 Publications, lectures, reports, conferences.
- 3-1 Monthly Report dated February 15, 1953.
- 3-2 Conference Rice Institute Houston, Texas February 20, 1953. Mr. Bechtold - Mr. Gentile - Mr. McDaniel.
- 3-3 Monthly Report dated March 11, 1953.

4-0 Factual Date

4-1 <u>Introduction</u>

The useful life of Selenium Rectifiers is limited by an increase of the internal resistance in the forward direction of the current - (ageing).

The rate of ageing is dependent upon several environmental and operating factors - ambient temperature, current density in the cells, and input voltage being the most important. The fabrication technique, the cell size, the method used in grading the finished product, appear also to have a certain influence on the long life behavior of rectifiers.

To evaluate the effect of the known ageing factors and to recognize other possible influences, the program of this investigation was designed to insure the maximum possible control on each of the known ageing parameters.

Three stack sizes for each of the three recognized manufacturing techniques are being studied, conducting in effect, 9 separate and parallel investigations. Five samples of each type of stack are employed to minimize the effect of individual differences.

Because of the high acceleration of ageing desired (from 3000 to 200 h) and of the desirable simplicity of a method based on temperature and current density, these factors are investigated first.

The preliminary objectives may be succintly stated in the following manner:

- (1) Determine, experimentally, the trend of ageing for stacks operating under rated conditions. This group of stacks will be referred to as the "Control Group".
- (2) Determine, experimentally, the current density (as a percentage of the rated current density) capable of accelerating the process of ageing to such an extent to simulate in the shortest possible time (tentative goal 200 h), 3000 h of operation under normal conditions.
- (3) Determine, experimentally, the ambient temperature capable of accelerating the process of ageing to such an extent to simulate in the shortest possible time (200 h, tentatively) 3000 h of operation under normal conditions.

4-2 Procurement of the Stacks

A total of 237 stacks has been procured from the three manufacturers selected in accord with the Contracting Agency. The three recognized fabrication techniques (pressed powder, evaporation, and molten dip) are represented, each in three commercial sizes. The specifications were:

Full wave bridge stacks, connected 4-1-1, rated 22-28 V_{ac} input, normal spacing, commercial coating, rated for fixed resistive load, at 35°C for the following approximate ratings:

.450 mA 2.75 A 9.5 A

were supplied.

Code	Process	Cell Size inches	Plate Spacing	No. of Stacks Procured
A ₃	p.p.	5x6	5/8	20
A ₂	p.p.	3 × 3	3/8	20
Aı	p.p.	1-1/4x1-1/4	1/8	40
B ₃	ev.	5 x 6	1/2	20
B ₂	ev.	3 ×3	3/16	20
B ₁	ev.	1-1/2x1-1/2	3/16	37
c ₃	m.d.	4-1/4 x6	5/16	20
C ₂	m.d.	3-3/8 Dia.	5/16	20
c_1	m.d.	1-3/8 Dia.	3/16	40

4-3 Administration of the Stacks

A progressive serial number is assigned to each stack upon reception. The initial characteristics [V_{output} , I_{Rev} , $V_{sch-circuit}$], the disposition of the stack, and the final characteristics are recorded.

Table I shows the initial and final characteristics of all the stacks used up to March 31, 1953.

4-4 <u>Description of Facilities</u>

4-4-1 Room temperature tests (30° Ambient)

The complete description of the facilities employed to perform the tests at ambient temperature will be found in the I Quarterly Report. No significant changes were made to the original apparatus.

4-4-2 High Ambient Temperature Tests

The apparatus employed in performing the high ambient temperature tests has been described in the I Quarterly Report.

A thermostatically controlled switch has been added; should the ambient temperature rise above a prefixed limit, all the stacks will be automatically deenergized.

4-5 Recording and Interpretation of Data

Input and output voltage, Plate and Room temperature, Input and Output current are read and recorded regularly.

Curves of Voutput vs. time are drawn for every stack tested.

The data are recorded as shown in Table IV: Fig. (1) shows a sample curve of Voutput vs. time.

Only average and significant data are included in the present report. However, the individual data and the relative curves are kept in the Project's file.

They will be made available upon request approved by the Contracting Agency.

The make of the stacks is indicated by Code Letter (A - B - C): Appendix \underline{A} , separately enclosed to the report and marked Confidential, supplies the Code's key.

4-6 Control Group

The control group consists of 45 stacks (5 units for each of the 9 types) operating at room temperature (30°C), at rated load and rated input voltage.

The output voltage, corrected to 26 volts input by linear interpolation, is plotted vs. time in Figs. 2-3-4-5-6-7-8-9-10-11-12. A_1 , A_2 , C_1 , C_2 stacks exhibit marked similarity of behavior among the 5 units; in the other stacks more than one trend is evident.

A study was made to investigate possible relationship between the initial characteristics (I reverse and Vsch.circuit) and the slope of the curves Voutput vs. time: No significant correlation is apparent. For example - comparing stacks 1-2 with 3-4-5

	1	2	3	4	5	
Vout (initial)	21.2	21.09	20.65	20.60	20.72	
I _{Rev} (" ")	37.6	22	13.3	13.1	9•3	
V _{sch.c.} (" ")	3.66	2.92	2.95	2.93	2.96	
Plate temperature raise (initial)	17°	740	17°	21°	19°	
Vour (after 100 days)	20.53	20.40	19.42	19.63	19.43	
Vout (after 100 days)						
-	66.	30.5				
<pre>IRev. (" ") Vschc. (" ") Plate temperature raise (after</pre>	66.	30.5	21.8	20.2	12.4	

Higher reverse current and higher initial voltage seem to correlate with lower rate of ageing; while no apparent connection. exists between short circuit voltage and the slope of the Voutput curve. Comparing stacks 6-7-8-9-10:

	6	7	8	9	10
V _{out} (initial)	21.3	21.53	21.60	21.53	21.52
I _{Rev.} (" ")	29.9	8.5	27.3	20.7	7.6
V _{schc.} (" ")	2.25	2.29	2.10	2.08	2.21
Plate temperature raise (initial)		14°	14°	14°	14°

·	6	7	8	9	10
Vout (after 100 days)	21.03	21.16	21.23	21.15	21.28
ÎRev. (" ")	20.5	10.0	29.7	24.6	11.3
V _{schc.} (" ")	2.09	2.12	2.02	2.07	2.05
Plate temperature rise (after 100 days)	10°	90	11°	12°	10°

Stacks 7 and 10 do not show any appreciable difference in ageing with respect to 6-8-9 regardless of the comparatively lower I_{Rev} and higher V_{output} . The investigation was extended to other stacks with the same negative results.

The discontinuity noticeable on some of the curves (Figs. 2-3-5-8-9-11) seems to point to a common external factor: on or about February 20, 1953, most of the stacks exhibited a sudden increase in output voltage. The secondary voltmeter chart did not show any apparent reason for the phenomenon, nor does the project's log indicate any abnormal event on or about that time.

Plate temperature and plate temperature rise vs. time were plotted for stacks 11-12-13 and 22-23-24-25-26. No significant trend was detectable and they are not included in the present report.

4-7-0 Tests at room temperature and higher than rated current density.

4-7-1 Three samples of each type, C3 excepted, were tested at ambient temperature rated input voltage, and 1.73 times rated current. Figs. 13-14-15-16-17-18-19-20 show graphically, voutput vs. time.

In general some qualitative correlation exists between those stacks and the corresponding control group.

For instance, the stacks A_3 , which exhibit marked differences in the control group, also show different rates of ageing when operated at $\sqrt{3}$ times rated current.

Even considering that the data from only 3 samples could be relied upon only to a certain extent, the average rate of ageing was considered too low to warrant further investigation, with the exception of stacks A₃. The test was suspended after 75 days to investigate the effect of higher current density.

4-7-2 Three samples of each small size (A₁-B₁-C₁) were tested at ambient temperature, rated input voltage, and 3 times rated current.

Stacks 101-102-103-122-124-128-34-35-36, Figs. 22-23 -

The Stacks Al aged rapidly and erratically: that is each one exhibited a different and variable rate of ageing. Not enough points were collected to warrant the drawing of a curve. The 3 stacks Bl showed definite uniformity of behavior and no appreciable drop in output voltage after 53 days. (Fig. 22): the test continues. The 3 stacks Cl aged considerably and regularly but each one in a different way. (Fig. 23).

Type A₁ seems to be affected to a point of rapid destruction. Type B₁ does not show appreciable effect, and type C₁ exhibits a definite trend.

Three more A_1 (63-64-74) were tested at $\sqrt{5}$ times rated current (Fig. 21): they aged consistently but at an unsatisfactory slow rate.

4-8-1 Test at rated Input voltage, rated current, and high temperature. (90° Ambient)

Eighteen stacks (3 A_1 , 3 A_2 , 3 A_3 , 3 B_3 , 3 C_1 , 3 C_2) were simultaneously tested at 90°C ambient temperature, at rated current, and rated input voltage. Surves 24-25-26-27-28-29 show, graphically, output voltage vs. time.

Only the A₁ stacks exhibited enough similarity of behavior to warrant the averaging of the data among the 3 samples.

All the others showed different rates of ageing for each unit; no generalization was possible. The test was interrupted after 26 days by a sudden rise in the ambient temperature (above 150°C) with consequent destruction of all the stacks. Each stack was individually protected on the input with fuses and the cooling apparatus was found in good operating condition. The only explanation for the sudden rise seems to be a rapid and simultaneous increase of the heat losses of the stacks, due to ageing.

A circuit breaker, thermostatically controlled, was added on the power input line to disconnect all the stacks should the temperature rise above a prefixed limit.

4-8-2 75°C Ambient Test

Six stacks (3 A₁ and 3 B₁) were tested at rated input voltage, rated output current, and 75°C ambient temperature.

The stacks A_1 (Fig. 30) exhibited considerable individual differences: stacks B_1 (Fig. 31) showed similarity of behavior. The test continues.

- 4-9-0 Investigation of stacks, operating inside of a small thermally insulated enclosure.
- 4-9-1 This test was originally conceived to study the effects of high plate temperature on forward resistance.

In the tests at high plate temperature, the effect of ageing on the output voltage is partially offset by the decrease in resistivity due to the rise in temperature.

When a stack is operating under load inside of a small Dewer Flask, the plate temperature rises rapidly because of the poor heat transfer coefficient of the enclosure.

Fig. 23 shows V_{output} vs. plate temperature for a C_1 stack operating at rated V_{input} and I_{output} ?

However, as shown in Fig. 33, the stack exhibits considerable ageing in a comparatively short time.

It did appear then, that a procedure based on this principle could be devised to accelerate the ageing of the stacks.

The simplicity and short duration of a test of this type are such that a further study seems to be justifiable.

5-0 <u>Conclusions</u>

The control group (5 units for each type) exhibited a rather uniform ageing among stacks of the same type with the exception of A3 and C1, where more than one trend is evident.

However, at the end of the period covered by the present report, after about 160 days of operation, individual differences are becoming evident.

It appears that, although the ageing is rather uniform in the early period of life, later the individual differencesamong the stacks become more and more pronounced.

This observation is confirmed by the results of the accelerated test, especially when the rate of ageing is considerably increased (Fig. 23).

The tests at 1.73 times rated current (4-7-1) and 75°C ambient (4-8-2) showed very little ageing.

In general the results of all the tests indicate more individual deviations than expected. All the tests which have shown promising results will have to be confirmed on a much larger number of stacks.

6-0 Program for the next interval

The life test of the control units will be continued.

The test at three times rated current will be performed on all the other types of stacks $(A_2-A_3-B_2-B_3-C_2-C_3)$ (three of each). Another set of A_1 will be tested at three times rated current to confirm rapid ageing of the first units tested.

Stacks B₁ and C₁ will be tested at four times and 3.5 times rated current, respectively.

The Dewar Flask test will be performed on all the small stacks: in case of promising results, a testing apparatus will be built to consent the test of more than one stack at the time.

7-1	Gentile, Ralph G.
	Dr. El. Eng University ef Rome (Italy) - 1938 Lieut. Eng. Italian Air Forces - Research and Dev 1939-1942 Research Engineer - F.A.T.M.E Rome (Italy) 1942-1943 Research Engineer - U.S. Government - Newport (R.I.) - 1943-1944 Chief Engineer - T.R.M. El. Co Middletown (Conn) 1944-1949 Assistant Professor Electrical Engineering - The Rice Institute - 1949 -
	Hours of work performed during present quarter 300
7-2	McDaniel, George
	B.A The Rice Institute, Houston, Texas - 1952 Summer Employment - Sun vil Co Electric and Communication Department 1948 - 1949 - 1950 - 1951 Graduate Student working toward a Master of Science Degree in Electrical Engineering at the Rice Institute Hours of work performed during present quarter
7-3	Smythe, Robert C.
	B.A The Rice Institute, Houston, Texas - 1952 <u>Summer Employment</u> - Trans-Texas Airways, Communication Department Working toward Bachelor of Science Degree in Electrical Engineering
	Hours of work performed during present quarter 200

Identification of Key Technical Personnel

7-0

TABLE I

			•	•	•	•		• -
Stack No.	Initial V out	Charactar I rev mA		Final V out	Characteris I rev mA		Test	Туре
1	21.20	37.6	2.66		•		Control	A3
2	21.08	22.1	2.92				n n	A3
2	20.65	13.3	2.85				n n	A3
3	20.60	13.1	2.83					A3
7	20.72	9.3	2.96					
5	21.50	29.9	2.25				H H	A3 A2
•	21.53	8.5	2.28					
7 8	21.60	22.2	2.10					A2
9		20.7	2.08				H H	A2
	21.53	7.6	2.21					≜2
10	21.52 20.86	3.54					* *	A2
11 12		2.80	2.55 2.51					Al
	20.59	3.82	2.60					Al
\mathfrak{B}	20.82	3.02						Al
14	20.63	2.66	2.38	35 15	-			Al
15	20.32	2.89	2.68	15.60	5	6.55	** **	Al
16	21.25	6.44	2.30				# #	Bl
17	21.26	6.49	2.63				• •	Bl
18	21.48	29.9	2.45					B2
19	21.43	20.8	2.28				* *	B2
20	21.24	181.	2.86				n n	B3
21	20.90	99•	3.37					B3
22	20.89	28.9	2.56					Cl
23	20.74	21.9	2.77				n n	Cl
24	20.89	33•3	2.73				**	Cl
25	20.57	26.0	2.92					Cl
26	20.79	33.2	2.77				19 19	Cl
27	21.46	148.	2.45					C2
28	21.27	130.	2.68				н н	C2
29	21.30	130.	2.62				н н	C2
30	21.01	118.	2.95					C2
31	21.30	148.	2.76					C2
32	-	•	•					
3 3	20.42	19.2	2.70				31	Cl
34	20.18	12.6	3.11	19.40	17.5	3.68		Cl
35	20.28	26.8	3.02	19.00	26.5	4.26	3	Cī
36	20.02	28.2	3.15	19.60	38.0	3.28	3 3 3	Cl
36 37 38 40	-	•	•		•	_	-	
38	20.11	16.8	3.25	19.30	27.0	3.92	*/3	Cl
40	21.50	33. 3	2.12	20.20	14.0	2.96	√ 3	A2
50	21.50	29.8	2.00			,	Control	
51	21.45	58.0	2.03				H H	B1
52	20.60	20.9	2.80	19.60	9.0	3.62	<i>ъ</i> ∕3	B1
53	21.60	70.3	2.00				Control	Bl
54	20.95	21.0	2.60	20.00	15.0	3.20		Bl
55	20.65	5.73	2.79	20.00	16.0	3.24	1 /3	Bl
57	20.59	8.7	2.85	19.00	20 Destroyed	4.12	750	Rì
61	21.50	21.5	1.96		Destroyed			AI
62	20.00	27.5	2.71		Shorted		750	A 1
63	21.60	4.0	1.95		21101 00U		1/5	Al
64	21.30	10.0	2.12				15 15	Al
65	21.60	8.7	1.20		Destroyed		900	Al
-,					~ a a or older		, 0	VT.

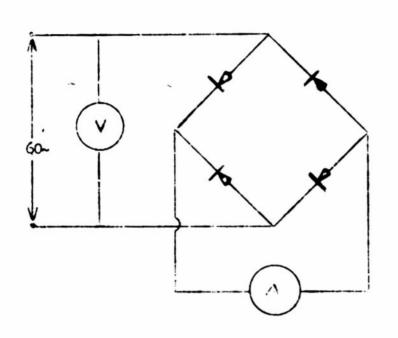
TABLE I - CHARACTERISTICS OF STACKS (Continued)

Stack	Initial	Cheracter	istics	Final	Characteris	tics		
No.	V out	I rev mA	V.sc.	V out	I rev ma	V.sc.	Test	Туре
66	21.50	7.4	2.00		Destroyed		90°	Al
67	20.24	29.5	3.03	18.50	26.0	4.80	Thermos	
68	19.78	19.8	3.36				Thermos	Cl
69	20.20	32.0	3.10				11 11	Cl
70	20.60	25.0	2.97		Destroyed		900	Cl
71	20.95	30.0	2.37		n n		90 °	Cl
72	20.40	39.6	3.20		m m		900	Cl
7 3	21.31	6.55	2.08	20.45	4.0	2.68	√ 3	Al
74	21.32	4.6	1.80				√5	Al
75							750	Al
76		•••					√ 3	A1
83	21.04	63.0	2.26	19.60	50.0	3.32	√ 3	A3
84	21.40	90.9	2.79	19.40	460.	3.44	√ 3	A 3
85							√ 3	Cl
86	21.30	133.	2.62		Destroyed		90°	C2
87	21.40	108.	2.38		n n		900	C2
88	20.60	120.	3.12		99 19		900	C2
89	20.50	102.	-	19.60	193.	3.42	√ 3	C2
90	20.59	93.0		19.70	208.	3.30	√ 3	C2
91	20 .80	18.5	2.84		Destroyed		90°	A 3
92	21.00	16.5	2.76		n n		900	A3
93	21.00	15.0	2.82		11 11		90°	A 3
94	21.00	15.0	2.94	17.58	18.4	5.21	√ 3	A 3
95	21.00	21.1	2.99	16.50	10.0	6.00	√ 3	A 3
9 6	21.20	12.9	2.00	18.30	6.0	4.80	√ 3	A2
97	21.16	10.2	-	19.80	9.0	3.26	√3 √3	A 2
98	21.60	22.0	2.00		Destroyed		900	A2
99	21.50	21.5	2.08		11 11		900	A2
100	21.60	23.0	2.03		M H		900	A 2
101	20.90	2.81	2 . 37	9.00	1494.	5.00	3 I	Al
102	20.67	1.33	2.35	17.90	1.0	4.98	3 I	Al.
103	20.80	3.10	2.36	17.80	1.0	4.81	3 I	Al
104	21.00	5.90	2.25	17.40	4.0	5.07	√3	Al
105	20.50	1.00	2.53		Shorted		7 <i>5</i> °	Al
106	20.95	22.8	3.30		Destroyed		900	B3
107	21.40	9 6.	2.80				Control	B3
108	21.00	29.9	3.25		Destroyed		90°	B3
109	21.40	20.3	2.76				Control	B3
110	21.50	123.	2.66				11 17	B3
111	21.00	101.	3.20		Destroyed		900	B3
112	21.00	109.	3.19	19.40	140.	3.86	√ 3	B3
113	20.95	77•	3.29	19.15	118.	3.98	√ 3	B3
114	21.37	139.	2.69	19.40	214.	3.60	√3	B3
115	20.78	29.5	2.86				Control	B2
116	20.95	23.1	2.71	20.00	26.0	3.40	√3	B2
117	20.85	38.3	2.71	19.70	40.0	3.64	√3	B2
118	20.78	30.0	2.79				Control	B2
119	20.85	29.5	2.74	20.15	40.0	3.38	√ 3	B2
120	21.00	17.4	2.66				Control	B2
121	20.48	17.1	3.02				Thermos	Bl
122	21.45	17.1	2.00	21.00	30	2.20	3	B1

TABLE I - CHARACTERISTICS OF STACKS (Continued)

Stack	Initial	Characteristics		Final	Characteri	Test	Type	
No.	V out	I rev mA	V.sc.	V out	I rev má	V.sc		
J.24	21.42	22.2	2.00	21.00	29	2.24	3	Bl
128	21.40	22.7	2.00	20.80	49	2.50	3	Bl
130	20.64	7.4	2.80	19.40	44	3.86	75°	Bl
131	21.40	8.9	2.06	18.90	114	3.68	Thermos	Bl
: 34	20.66	6.5	2.80	•			75°	Bl
-35	20.72	8.7	2.70				Thermos	Bl
337	21.15	399•	3.21				Control	C3
139	20.62	469.	3.21				11	C3
140	20.75	300.	3.07				n n	C3
149	20.61	312.	3.36				n n	C3
154	20.60	570.	3.21				n n	C3
159	20.30	104.	2.86				3I	C2
161	20.40	252.	2.84	16.80	343	6.80	31	C2
165	20.40	80.	2.72	19.60	184	3.56	31	C2
188	20.50	4.0	2.56				Thermos	Al
189	20.40	4.0	2.52	16.98	520.	3.45	rt 11	Al
190	20.55	5.0	2.58	15.60			n n	Al
191	20.60	6.0	2.24				31	Al
192	20.48	5.0	2.40	16.9	14	5.95	31	A1
193	20-52	5.0	2.40	•		-	31	A1
194	20.40	4.0	2.42	19.35	234.	3.40	Thermos	11
208	21.10	14.0	1.97	20.80	4.0	2.40	16 11	D1

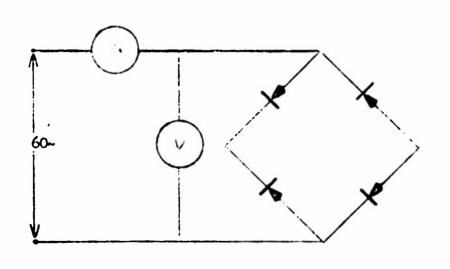
TABLE II TEST CIRCUIT FOR FORWARD CONDUCTANCE TEST



NOTES:

- Voltmeter, C5A. Weston Model:155, 0-5 volts.
- Ammeter, B4B, Weston Model 45, 0-1.5, 0-3, & 0-15 amperes, with External Shunts

TEST CIRCUIT FOR REVERSE CURRENT TEST



NOTES:

- Voltmeter, S21.
 Weston Model 341,
 0-30 & 0-60 volts
- Milliammeter, L4A. Weston, Model 433, 0-50 & 0-100 mA.

or

Milliammeter, L5A, Weston, Model 433, 0-250 & 0-500 mA.

TABLE III

LIST OF METERS USED

VOLIMETERS:

S21	WESTON, Model 341, 0-30 & 0-60 Volts.
A9C	WESTON, Model 45, 0-30, 0-150 & 0-300 Volts.
C5A	WESTON, Model 155, 0-5, 0-24, 4 0-120 Volts.
\$22	WESTON, Model 341, 0-7.5 & 0-15 Volts.

AMMETERS:

LIE	WESTON, Model 622, 0-2, 5, 10, 20, 50, 100, 200, 500 mA.
DBC	WESTON, Model 433, 0-10 & 0-20 Amps.
B4B	WESTON, Model 45, 0-1.5, 0-3 & 0-15 Amps.
LAA	WESTON, Model 433, 0-50 & 0-100 mA.
L5A	WESTON, Model 433, 0-250 & 0-500 mA.
Blib	GENERAL ELECTRIC, Model BDP9ACW1, 0-2, 0-10 & 0-50 Amps.
B12B	GENERAL ELECTRIC, Model 3DP9ACW1, 0-2, 0-10 & 0-50 Amps.

POTENTIOMETERS:

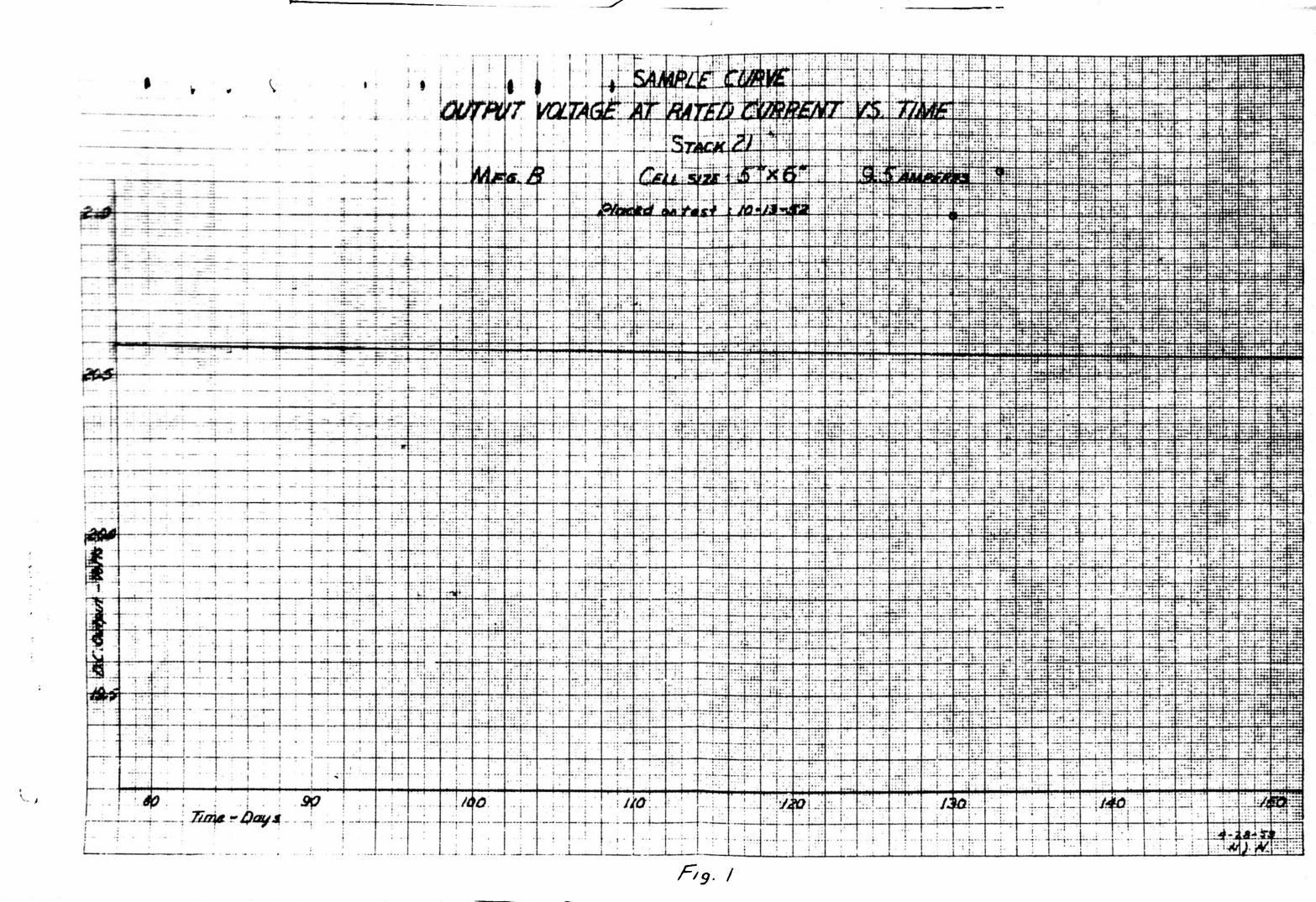
K2E LEEDS & NORTHRUP Thermocouple Potentiometer, 0-200°C.

TABLE Y

CODE	CELL SIZE (In. x In.)	RATED CURRENT (AMPS)	(AMPS)	√3 I _r (AMPS)	3 I _T
A 1	1-1/4 x 1-1/4	0.45	.78	1.0	1.35
A ₂	3 x 3	2.75	4.75	•	
4 ₃	5 x 6	9.5	16.5		***
B 1	1-1/2 x 1-1/2	0.75	1.3		2.25
B ₂	3 × 3	2.75	4.75		
B ₃	5 x 6	9•5	16.5	-	
c_1	1-3/8 dia.	0.45	.78	***	1.35
c ₂	3-3/8 dia.	2.75	4.75		
c ₃	4-1/4 x 6	9.5			***

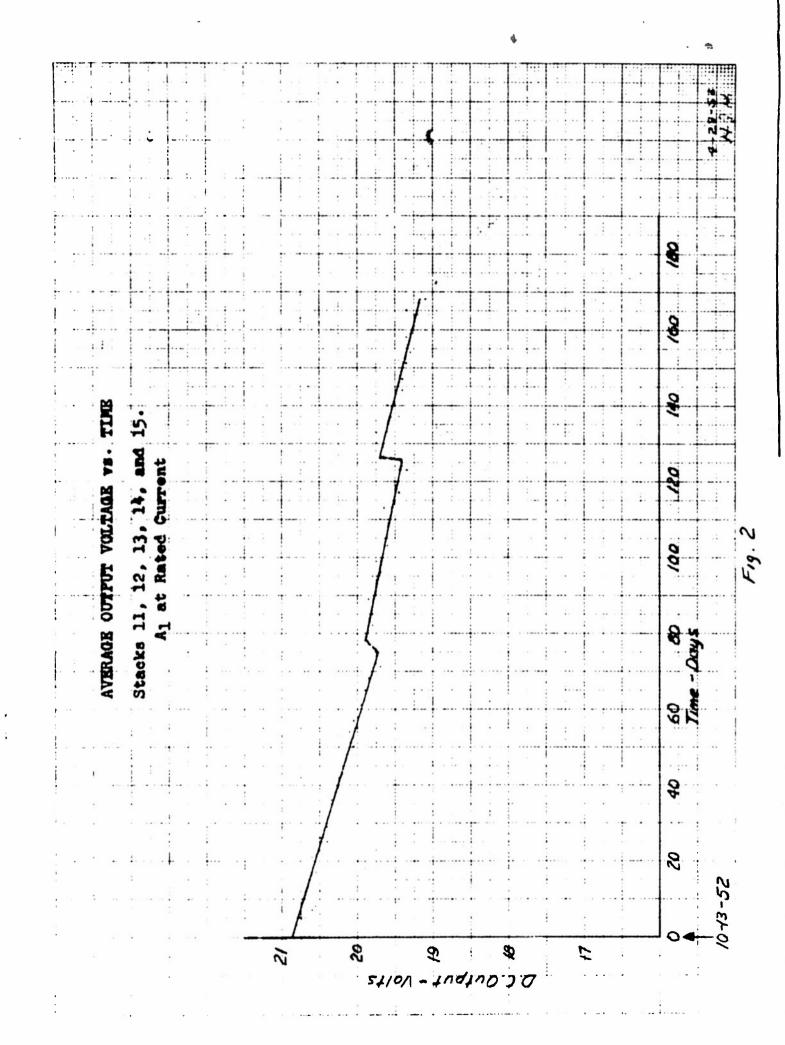
	POSITION	DATE	TIME	TIME ELAPSED	V INPUT	v ourpur	I OUTPUT	I INPUT	I OUTPUT I	v outpur	PLATE CO	ROOM CO	I. REV. mA	V.SCH.C	V INPUT CORRECTED TO 26 V.		OPERATOR	STACK NO. 21 POSITION 2 MFG.NO CODE B3 RATED V 26.00 RATED I 9.5
METERS					S21	A9C	BllB	D8c	B11B	A 9C	K2E	K2E	L4A L5A S21	Ĺ5Ŧ				
		1-17 1-20 1-20 1-24 1-24 1-31 2-3 2-3 2-7	1300 1300 1300 1300 1500 1700 1330 1300 1330 1330 1400 1300 1300 13	82 82 84 85 85 89 91 92 96 99 103 113 117 123 126 126 127 130 130 133	25.15 25.90 25.40 25.25 25.10 25.14 24.92 24.91 25.45 25.10 25.35	20.20 19.90 20.20 20.70 19.90 19.95 19.95 19.93 19.80 19.80 19.70 20.10 19.80 20.10 19.60 20.00 20.40 20.00	9.73 9.70 9.30 9.32 9.32 9.27 9.15 	10.36		19.9	47.5 48.0 48.0 45.0 46.5 49.5 50.0 46.0 50.0	29.7 32.7 30.7 28.5 32.2 30.0 31.0 30.5 32.5 29.5 27.0 31.5	106	3.29	20.57 20.77 20.58 20.55 20.62 20.60 20.60 20.50 20.60 21.14		A.A. A.A. A.A. A.A. A.A. A.A. A.A. A.A	

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	POSITION	DATE	TIME	TIME ELAPSED	V INPUT	V OUTPUT	I OUTPUT	I INPUT	I OUTPOT I	V COTPUT US	PLATE C°	ROCH C.	I. REV.mA	V.SCH.C	V INPUT CORRECTED TO 26 V.		OPERATOR	MFG.NO CODE B3 RATED V 26.00 RATED I 9.5
METERS																		NOTES
		2-27 3-6 3-6 3-7 3-10 3-13 3-16 3-17 3-20 3-23 3-24 3-27 3-30 3-31	3010	165	25.25 25.55 24.90 25.25 26.00 25.60	19.90 19.85 19.95 20.20 20.10 19.85 20.00 20.40 20.20 20.31 20.20	9.55 9.50 9.5 9.70 9.60 8.75	10.85			48.7 49.0 50.5 49.0 51.0 52.0	35.0 34.0 31.0 32.0	101		20.60 20.60 20.62 20.62		P. P. P. H. H. H. H. H.	lightened loose connection to bus.) 3-7-53 R.S.



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DC. Output - Volts

AVERAGE DUFFUT VOLLTAGE VS. TIME

Stacks 63, 64, and 74

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Fig. 28

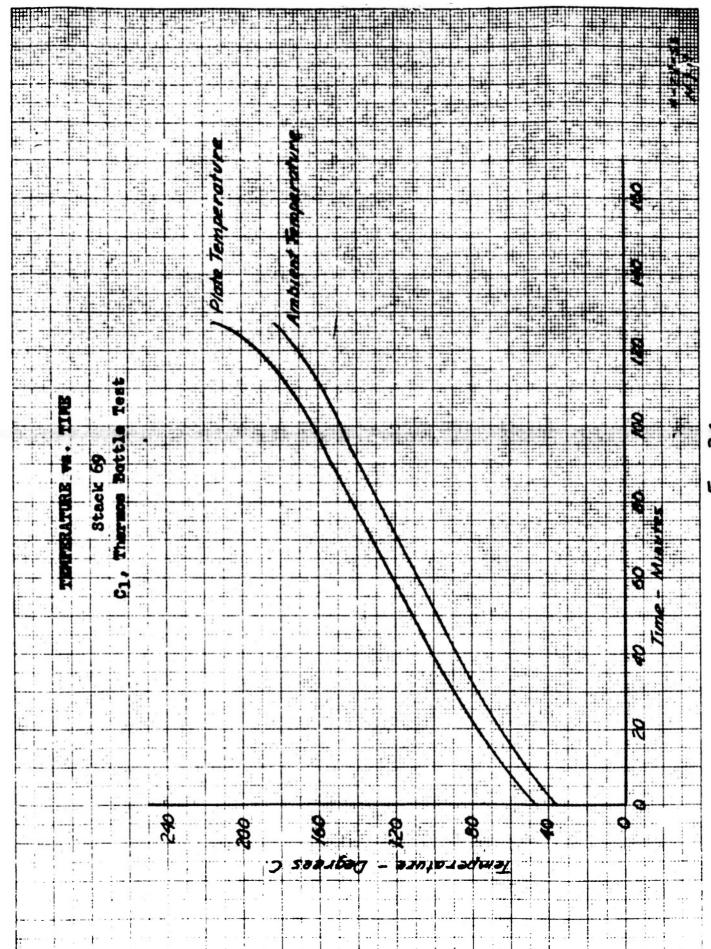
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